

전파 간섭계

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서울대학교 평창캠퍼스
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권우진
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Radio observations

- To achieve 1 arc-second resolution
at $\lambda = 500 \text{ nm}$: $D \sim 10 \text{ cm}$
at $\lambda = 1 \text{ mm}$: $D \sim 200 \text{ m}$
- Difficulties in building a big radio telescope:
 1. The required tracking accuracy $\sim \theta/10$ but the best mechanical tracking and pointing accuracy $\sim 1''$ due to
 - Gravitational sagging
 - Antenna deformations caused by differential solar heating
 - Wind gusts
 2. Surface accuracy $\sim \lambda/20$

$$\theta \sim \lambda/D$$

What radio interferometers look like?

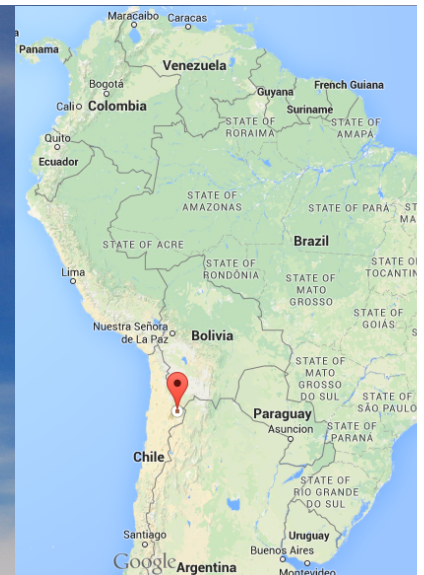
- Arrays: e.g., JVL, SMA, NOEMA, ALMA
- Very Long Baseline Interferometers: e.g., KVN



ALMA 2017 July 14 Woojin Kwon

Atacama Large Millimeter/submillimeter Array

- The largest ground-based astronomical facility
- 50 12-m, 12 7-m, 4 12-m = 66 antennas
- ~5000 m in altitude, Chajnantor plateau, Chile
- East Asia, Europe, North America, & Chile
- <https://almascience.org>



ALMA 인류 역사상 가장 규모가 큰 천문대



ALMA 인류 역사상 가장 규모가 큰 천문대





References

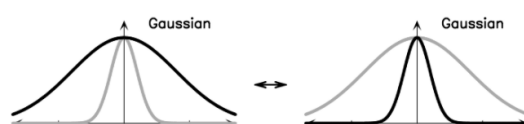
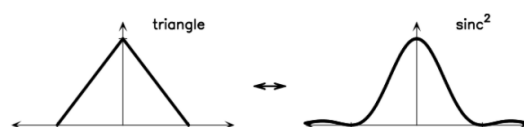
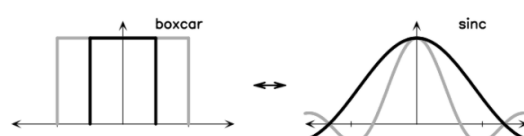
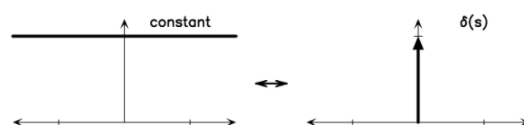
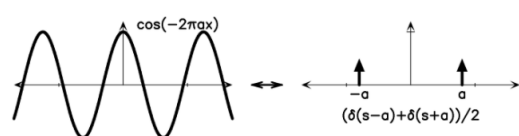
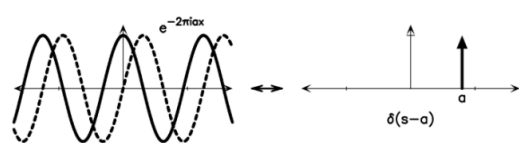
- **Essential Radio Astronomy (3.7)**
J. J. Condon and S. M. Ransom, NRAO
<https://science.nrao.edu/opportunities/courses/era/>
- Fundamentals of Radio Astronomy (ch. 5, 6)
J. M. Marr, R. L. Snell, and S. E. Kurtz
- Tools of Radio Astronomy
K. Rohlfs and T. L. Wilson
- Interferometry and Synthesis in Radio Astronomy
A. Richard Thompson, James M. Moran, and George W. Swenson, Jr.
- Synthesis Imaging in Radio Astronomy
Astronomical Society of the Pacific Conference Series (Volume 180)



Fourier transform

$$F(s) \equiv \int_{-\infty}^{\infty} f(x) e^{-2\pi i s x} dx,$$

$$f(x) \equiv \int_{-\infty}^{\infty} F(s) e^{2\pi i s x} ds,$$



Fourier transform

$$F(s) \equiv \int_{-\infty}^{\infty} f(x) e^{-2\pi i s x} dx,$$

$$f(x) \equiv \int_{-\infty}^{\infty} F(s) e^{2\pi i s x} ds,$$

$$f(x) + g(x) \Leftrightarrow F(s) + G(s).$$

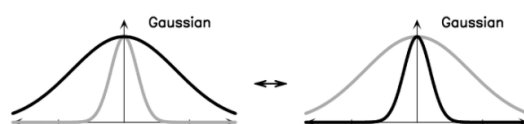
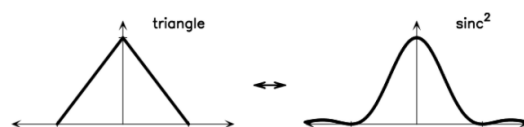
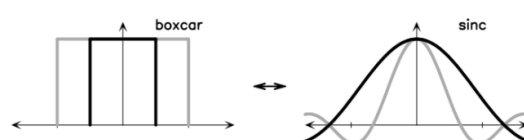
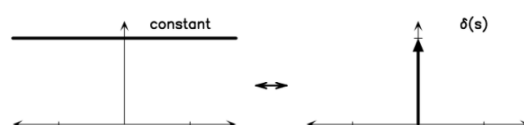
$$af(x) \Leftrightarrow aF(s).$$

$$f(x-a) \Leftrightarrow e^{-2\pi i a s} F(s).$$

$$f(ax) \Leftrightarrow \frac{F(s/a)}{|a|}.$$

$$f(x) \cos(2\pi \nu x) \Leftrightarrow \frac{1}{2} F(s-\nu) + \frac{1}{2} F(s+\nu).$$

$$\frac{df}{dx} \Leftrightarrow i2\pi s F(s).$$

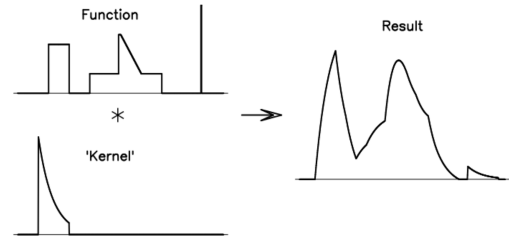


Convolution & Cross-correlation

• Convolution

$$h(x) = f * g \equiv \int_{-\infty}^{\infty} f(u) g(x - u) du.$$

$$f * g \Leftrightarrow F \cdot G. \quad \text{Convolution theorem}$$



• Cross-correlation

$$f \star g \equiv \int_{-\infty}^{\infty} f(u) g(u - x) du.$$

$$f \star g \Leftrightarrow \overline{F} \cdot G. \quad \text{Cross-correlation theorem}$$

Auto-correlation

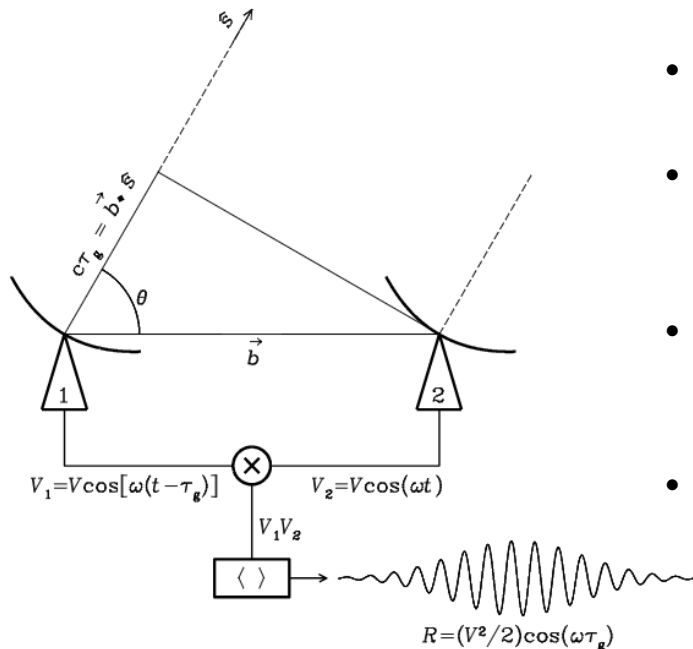
$$f \star f \Leftrightarrow \overline{F} \cdot F = |F|^2.$$

Wiener-Khinchin theorem

FOV & θ_s of interferometers

- Optical telescopes:
detectors with millions of pixels
- Radio single dish antennas:
one or a small number of receivers
(e.g., TRAOS SEQUOIA with 16 pixels)
- Interferometers:
e.g., ALMA 12 m antennas over 12 km in Band 6 (~ 1.2 mm)
FOV $\sim \lambda/D \sim 20''$
 $\theta_s \sim \lambda/(\text{longest baseline}) \sim 0.02''$
 $\Rightarrow 10^6$ "pixels"

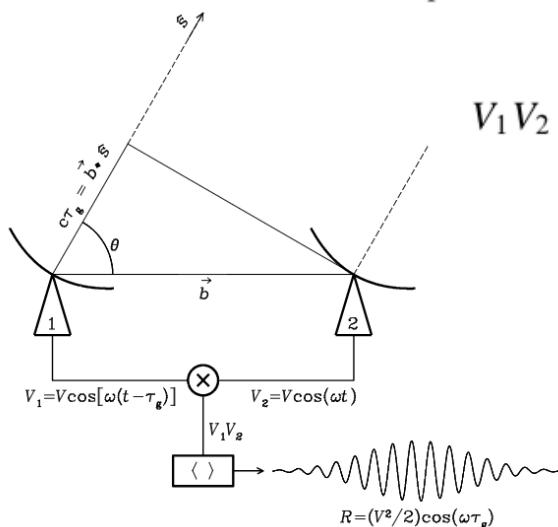
Quasi-monochromatic 2-element interferometer



- “General” case!
- Quasi-monochromatic condition: $\Delta\nu \ll 1/\tau_g$
- **Correlator**: multiply and time-average
- **Geometric delay**: $\tau_g = \frac{\vec{b} \cdot \hat{s}}{c}$

Output of correlator

$$V_1 = V \cos[\omega(t - \tau_g)] \quad \text{and} \quad V_2 = V \cos(\omega t).$$



$$\begin{aligned} V_1 V_2 &= V^2 \cos[\omega(t - \tau_g)] \cos(\omega t) \\ &= \left(\frac{V^2}{2}\right) [\cos(2\omega t - \omega\tau_g) + \cos(\omega\tau_g)] \end{aligned}$$

$$\cos x \cos y = [\cos(x + y) + \cos(x - y)]/2$$

$$\Delta t \gg (2\omega)^{-1}$$

$$R = \langle V_1 V_2 \rangle = \left(\frac{V^2}{2}\right) \cos(\omega\tau_g).$$

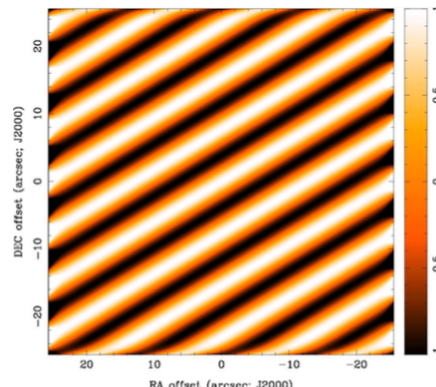
Fringes

- Fringes: sinusoidal correlator output
- Fringe phase

$$\phi = \omega \tau_g = \frac{\omega}{c} b \cos \theta$$

$$\left| \frac{d\phi}{d\theta} \right| = \frac{\omega}{c} b \sin \theta$$

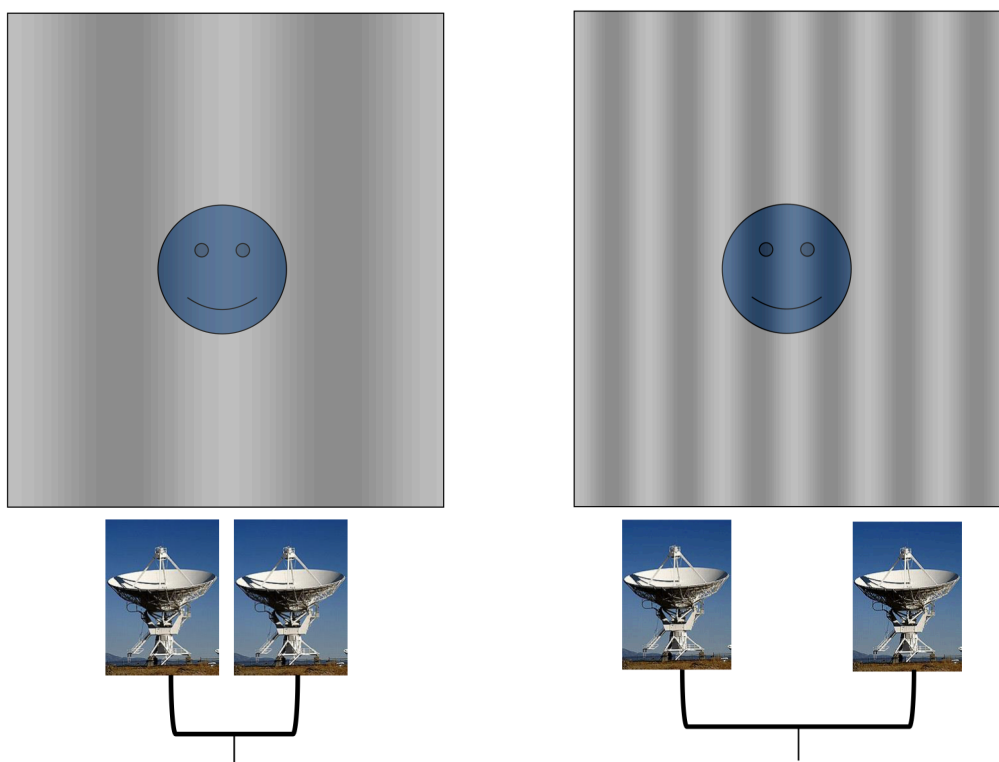
$$= 2\pi \left(\frac{b \sin \theta}{\lambda} \right)$$



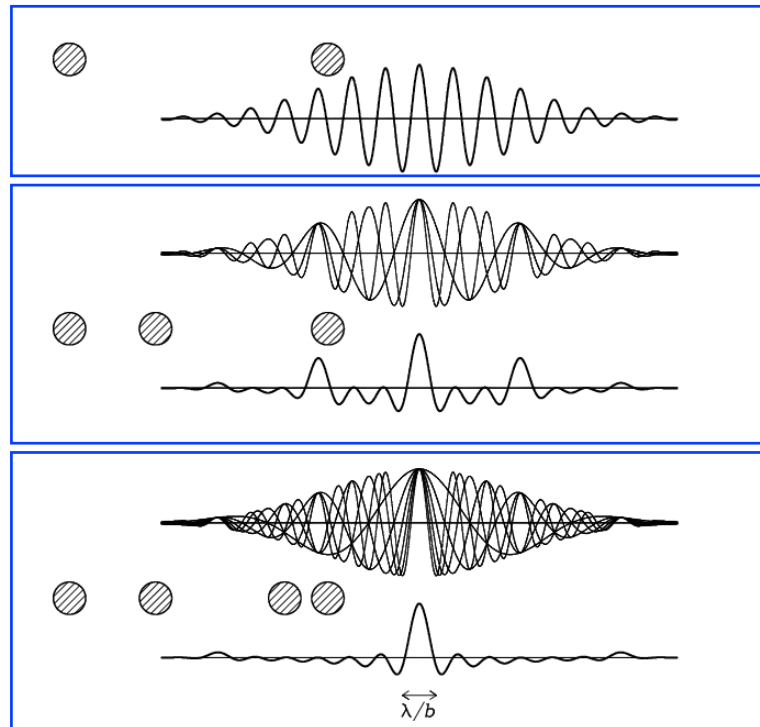
The **fringe period** $\Delta\phi = 2\pi$ corresponds to an angular shift $\Delta\theta = \lambda / (b \sin \theta)$.

Depending on projected baselines
Good image?

Sensitive Scales of Fringes



More antennas better image



Complex correlator

- Slightly extended sources ($I = I_E + I_O$)
 - “cosine” correlator sensitive to even (inversion symmetric) structure
 - “sine” correlator sensitive to odd (anti-symmetric) structure

$$R_c = \int I(\hat{s}) \cos(2\pi \vec{b} \cdot \hat{s}/\lambda) d\Omega = \int I(\hat{s}) \cos(2\pi \vec{b} \cdot \hat{s}/\lambda) d\Omega$$

$$R_s = \int I(\hat{s}) \sin(2\pi \vec{b} \cdot \hat{s}/\lambda) d\Omega$$

- Complex correlator: combination of cosine and sine correlators
cf. Euler's formula $e^{i\phi} = \cos \phi + i \sin \phi$

- Complex visibility**

$$\mathcal{V} \equiv R_c - iR_s$$

$$\mathcal{V} = Ae^{-i\phi}$$

$$A = (R_c^2 + R_s^2)^{1/2}$$

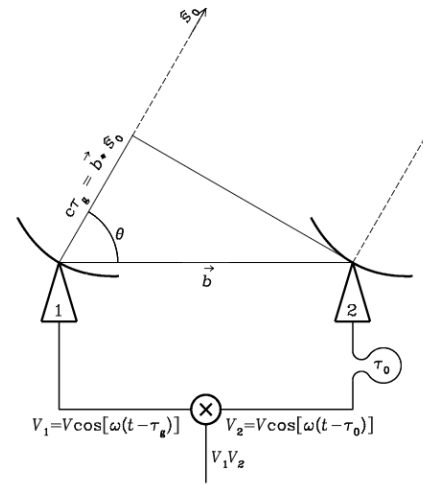
$$\phi = \tan^{-1} (R_s/R_c)$$

$$\mathcal{V} = \int I(\hat{s}) \exp(-i2\pi \vec{b} \cdot \hat{s}/\lambda) d\Omega$$

Bandwidth smearing

- Quasi-monochromatic interferometers
=> interferometers with finite bandwidths and integration times

$$\begin{aligned}\mathcal{V} &= \int \left[\int_{\nu_c - \Delta\nu/2}^{\nu_c + \Delta\nu/2} I_\nu(\hat{s}) \exp(-i2\pi \vec{b} \cdot \hat{s} / \lambda) d\nu \right] d\Omega \\ &= \int \left[\int_{\nu_c - \Delta\nu/2}^{\nu_c + \Delta\nu/2} I_\nu(\hat{s}) \exp(-i2\pi \nu \tau_g) d\nu \right] d\Omega. \\ \mathcal{V} &\approx \int I_\nu(\hat{s}) \text{sinc}(\Delta\nu \tau_g) \exp(-i2\pi \nu_c \tau_g) d\Omega.\end{aligned}$$



- Instrumental delay τ_0
to minimize the attenuation

$$|\tau_0 - \tau_g| \ll (\Delta\nu)^{-1} \quad \Delta\nu \Delta\tau_g \ll 1 \quad \Delta\nu (b \sin \theta) \Delta\theta/c \ll 1$$

$$c\tau_g = \vec{b} \cdot \vec{s} = b \cos \theta$$

$$|c\Delta\tau_g| = b \sin \theta \Delta\theta$$

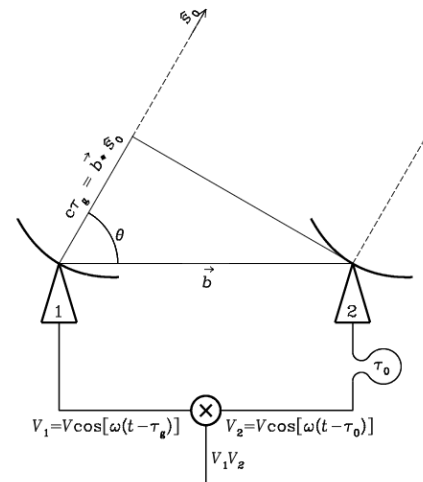
$$\theta_s \approx \lambda / (b \sin \theta)$$

$$\Delta\nu \ll \nu \frac{\theta_s}{\Delta\theta}$$

Bandwidth smearing

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- Instrumental delay τ_0
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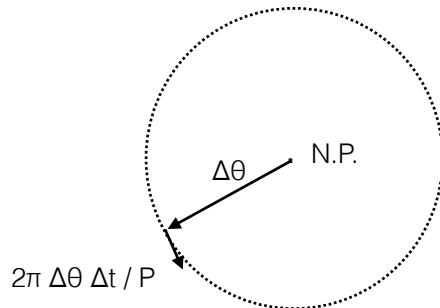
$$|\tau_0 - \tau_g| \ll (\Delta\nu)^{-1}$$

$$c\tau_g = \vec{b} \cdot \vec{s} = b \cos \theta$$

$$\Delta\nu \ll \frac{\nu \theta_s}{\Delta\theta} = \frac{1.5 \times 10^9 \text{ Hz} \cdot 4 \text{ arcsec}}{900 \text{ arcsec}} \approx 7 \text{ MHz.}$$

$$\Delta\nu \ll \nu \frac{\theta_s}{\Delta\theta}$$

Integration time smearing



$$P \approx 23^{\text{h}}56^{\text{m}}04^{\text{s}} \approx 86164$$

$$\frac{2\pi\Delta\theta\Delta t}{P} \ll \theta_s$$

$$\Delta t \ll \frac{\theta_s}{\Delta\theta} \cdot 1.37 \times 10^4 \text{ s}$$

$$\Delta t \ll \frac{\theta_s}{\Delta\theta} \cdot 1.37 \times 10^4 \text{ s} = \frac{4 \text{ arcsec}}{900 \text{ arcsec}} \cdot 1.37 \times 10^4 \text{ s} \approx 60 \text{ s.}$$

Visibility

- Now, assuming an interferometer with a negligible bandwidth attenuation
- Visibility: data of interferometers
(Fourier transform of an image)

Steering antenna with an instrumental delay

$$\mathcal{V} \approx \int I_\nu(\hat{s}) \text{sinc}(\Delta\nu \tau_g) \exp(-i2\pi\nu_c \tau_g) d\Omega.$$

$$\tau = \tau_g - \tau_i$$

Phase center s_0

$$\hat{s} = \hat{s}_0 + \hat{\sigma}$$

$$V \approx \int A(\hat{s}) I_\nu(\hat{s}) \exp(-i2\pi\nu\tau) d\Omega$$

$$= \int A(\hat{s}) I_\nu(\hat{s}) \exp\left[-i2\pi\nu\left(\frac{\vec{b} \cdot \hat{s}}{c} - \tau_i\right)\right] d\Omega$$

$$= \exp\left[-i2\pi\nu\left(\frac{\vec{b} \cdot \hat{s}_0}{c} - \tau_i\right)\right] \int A(\hat{s}) I_\nu(\hat{s}) \exp\left[-i2\pi\nu\left(\frac{\vec{b} \cdot \hat{\sigma}}{c}\right)\right] d\Omega$$

$$V = \int A(\hat{s}) I_\nu(\hat{s}) \exp\left[-i2\pi\nu\left(\frac{\vec{b} \cdot \hat{\sigma}}{c}\right)\right] d\Omega$$

Visibility

- Now, assuming an interferometer with a negligible bandwidth attenuation
- Visibility: data of interferometers
(Fourier transform of an image)

$$\mathcal{V} \approx \int I_\nu(\hat{s}) \text{sinc}(\Delta\nu \tau_g) \exp(-i2\pi\nu_c \tau_g) d\Omega.$$

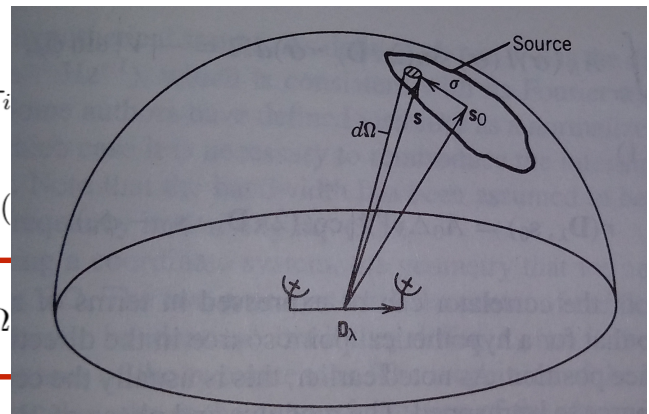
$$\begin{aligned} V &\approx \int A(\hat{s}) I_\nu(\hat{s}) \exp(-i2\pi\nu\tau) d\Omega \\ &= \int A(\hat{s}) I_\nu(\hat{s}) \exp[-i2\pi\nu \left(\frac{\vec{b} \cdot \hat{s}}{c} - \tau_i \right)] d\Omega \\ &= \exp[-i2\pi\nu \left(\frac{\vec{b} \cdot \hat{s}_0}{c} - \tau_i \right)] \int A(\hat{s}) I_\nu(\hat{s}) \exp[-i2\pi\nu \left(\frac{\vec{b} \cdot (\hat{s} - \hat{s}_0)}{c} \right)] d\Omega \\ V &= \int A(\hat{s}) I_\nu(\hat{s}) \exp[-i2\pi\nu \left(\frac{\vec{b} \cdot \hat{\sigma}}{c} \right)] d\Omega \end{aligned}$$

Steering antenna with an instrumental delay

$$\tau = \tau_g - \tau_i$$

Phase center s_0

$$\hat{s} = \hat{s}_0 + \hat{\sigma}$$



Interferometers in 3D

$$V = \int A(\hat{s}) I_\nu(\hat{s}) \exp[-i2\pi\nu \left(\frac{\vec{b} \cdot \hat{\sigma}}{c} \right)] d\Omega$$

$$2\pi\nu \frac{\vec{b}}{c} = 2\pi \frac{\vec{b}}{\lambda} = 2\pi(u, v, w)$$

$$\hat{\sigma} = (l, m, n)$$

$$d\Omega = \frac{dl dm}{\sqrt{1 - l^2 - m^2}}$$

$$V(u, v, w) = \int \int \frac{A(l, m) I(l, m)}{\sqrt{1 - l^2 - m^2}} \exp[-i2\pi(ul + vm + w\sqrt{1 - l^2 - m^2})] dl dm$$

$$\sqrt{1 - l^2 - m^2} \approx 1$$

$$V(u, v, w) = \exp(-i2\pi w) \int \int A(l, m) I(l, m) \exp[-i2\pi(ul + vm)] dl dm$$

Interferometer

$$V = \int A(\hat{s}) I_\nu(\hat{s}) \exp[-i2\pi\nu \left(\frac{\vec{b} \cdot \hat{\sigma}}{c} \right)] d\Omega$$

$$2\pi\nu \frac{\vec{b}}{c} = 2\pi \frac{\vec{b}}{\lambda} = 2\pi(u, v, w)$$

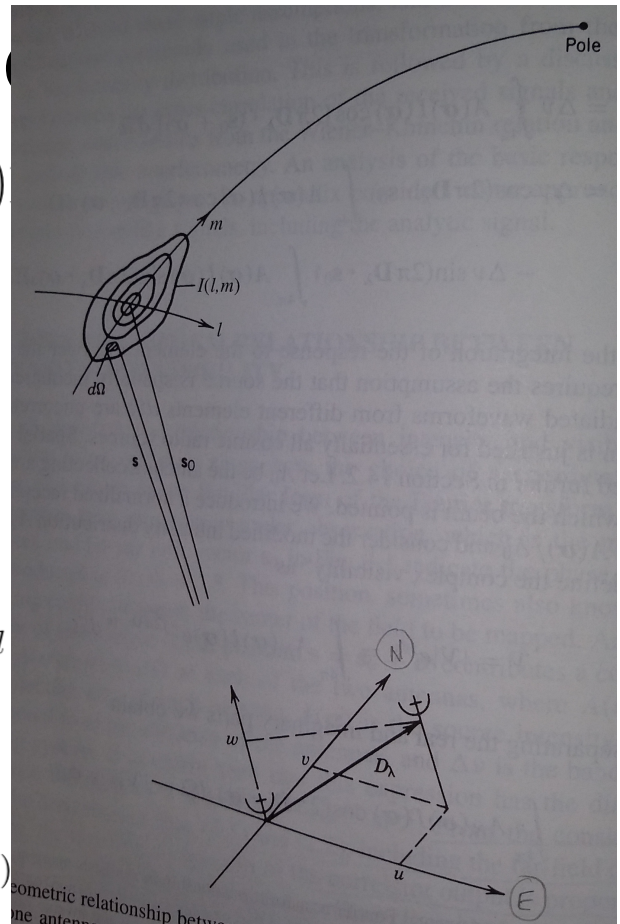
$$\hat{\sigma} = (l, m, n)$$

$$d\Omega = \frac{dl dm}{\sqrt{1-l^2-m^2}}$$

$$V(u, v, w) = \iint \frac{A(l, m) I(l, m)}{\sqrt{1-l^2-m^2}} \exp[-i2\pi(u l + v m + w n)] dl dm$$

$$\sqrt{1-l^2-m^2} \approx 1$$

$$V(u, v, w) = \exp(-i2\pi w) \iint A(l, m) I(l, m) \exp[-i2\pi(u l + v m)] dl dm$$



Visibility and Image

- (Inverse) Fourier transformation

On $w = 0$ plane:

$$V(u, v) = \iint A(l, m) I(l, m) \exp[-i2\pi(u l + v m)] dl dm$$

$$V(u, v) \Leftrightarrow A(l, m) I(l, m)$$

$$S(u, v) V(u, v) \Leftrightarrow FT^{-1}[S(u, v)] * FT^{-1}[V(u, v)]$$

$$S(u, v) V(u, v) \Leftrightarrow B_D(l, m) * [A(l, m) I(l, m)]$$

Sensitivity

- A single antenna

$$\sigma_S = \frac{2kT_s}{A_e(\Delta\nu \tau)^{1/2}}$$

- A two-element interferometer

$$\sigma_S = \frac{2^{1/2} kT_s}{A_e(\Delta\nu \tau)^{1/2}}$$

- A N-element interferometer: $N(N-1)/2$ independent pairs

$$\sigma_S = \frac{2kT_s}{A_e[N(N-1)\Delta\nu \tau]^{1/2}}$$

Interferometric observations

- Calibrators

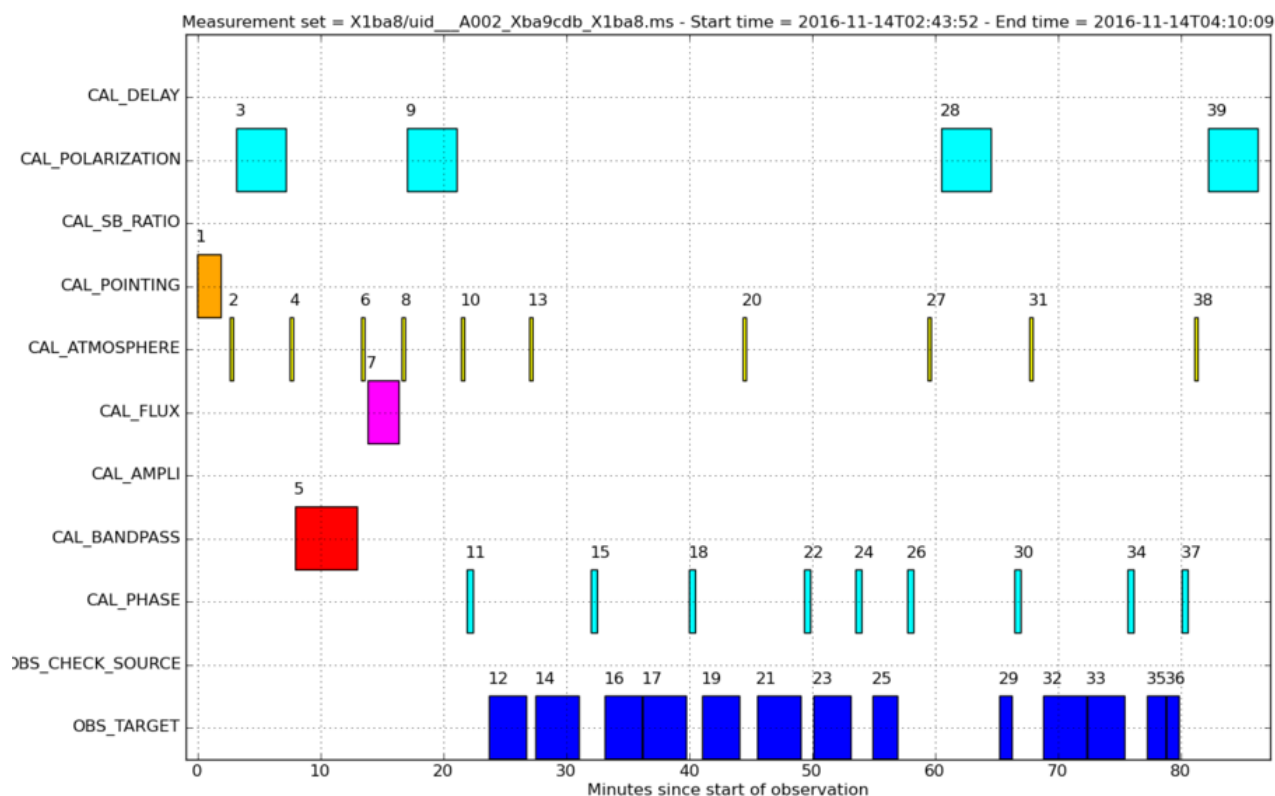
Flux (also called amplitude) calibrator

Bandpass calibrator

Phase calibrator

- A typical sequence

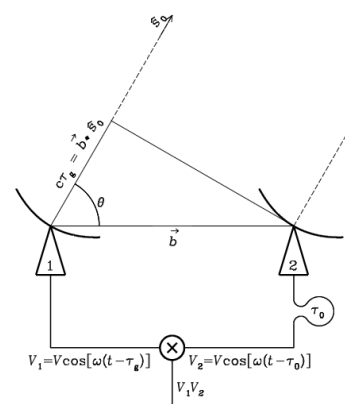
Flux cal. → Bandpass cal. → Phase cal. and science target cycles (e.g., 10 min period) → Last phase cal.



Observing Schedule

From raw data to image

- Calibration: to have all antennas phased up
 - Bandpass calibration
 - Flux (amplitude) calibration
 - Phase calibration
- Imaging: from calibrated visibilities to images
 - Inverse Fourier transform
 - Deconvolution
 - Primary beam correction



$$S(u, v) V(u, v) \Leftrightarrow B_D(l, m) * [A(l, m) I(l, m)]$$

Take-home messages

- Interferometry samples Fourier components of sky brightness: visibilities
- Images are made by Fourier transforming sampled visibilities
 - images are not unique
 - limited scales of detected structures due to missing visibilities

$$S(u, v)V(u, v) \rightleftharpoons B_D(l, m) * [A(l, m)I(l, m)]$$